DEVELOPMENT OF AN ELECTRIC SPRAYER FOR GREENHOUSE AND SMALL OPEN FIELD

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ABSTRACT

Hand-held and backpack sprayers are inexpensive tools used to apply pesticides on small acreages. Greenhouse, small vegetables field, small orchards, and tree plantations are examples of areas that often require pesticide applications to protect them from weeds, insects, and diseases. Effective pest control depends on applying the proper amount of pesticide. In greenhouse conditions inside are different from open field. The conventional sprayers, such as the self-propelled or tractor mounted boom sprayers are not suitable for a greenhouse conditions. The electric developed sprayer was evaluated, and its performance was investigated and compared to Suzuki 2.13 kW air assist knapsack sprayer. The experiments were carried out at during 2015/2016 seasons. The developed hydraulic sprayer may able to operate as vertical and horizontal boom sprayer. It's able to apply in piper crops in greenhouse and small field area of Cabbage (Brassica Oleracea var. Capitata) under Egyptian conditions. The results showed that the horizontal boom set gave high value of deposition compared to vertical boom set. As well as, the increasing of operating pressure tends to increase the deposition values for developed solar sprayer. The deposit spray values under open field conditions were 0.133μg/cm^2, 0.187μg/cm^2 and 0.208μg/cm^2. The coverage values under open field conditions were 37.8%, 39.1% and 44.5% for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. As well as, the coverage percent values under greenhouse conditions were 27.8 %, 29.7% and 33.8 % for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. The power consumed was 0.263 kW, 0.289 kW and 0.300 kW at 125 kPa, 150 kPa and 200 kPa respectively. As well as the battery power reduction rate were 0.051 and 0.164 with PV panel charger under small open field and greenhouse after one hour operating time respectively.

Keywords: *sprayer, greenhouse, electrical sprayer.*

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INTRODUCTION

The use of pesticides is an integrant part of the modern agriculture and contributes to productivity and quality of crop grown (Hilz & Vermeer, 2013). Oerke (2006) reports that the use of pesticides prevents yield losses up to 45 % of the of the world food supply. However, the pesticides must be applied with care in order to achieve the objective of the pesticides application technology, which consists in pest and diseases control with minimal environmental contamination and without leaving residues on foods. An automatic spraying system could be set to begin operation at night ensuring that the plants are sprayed in conditions that cause the least amount of damage to the human and plants (Sammons et al.,2005). Also they described an autonomous spraying robot with navigation control based on inductive sensors which detect metal pipes buried on the ground. Rowe el. al, (2000) mentioned that; if an automated system for pesticide application is used in lieu of hand spraying, most of the hazards and discomfort for the handler is eliminated. One system which is available is the Dramm Autofog (Hummert International, Earth City, CO.). This unit applies commonly used pesticides using an "automatic aerosol micro-particle generator" and a circulating fan. These specialized unit costs about $5000, which may be prohibitively expensive if several units, are needed for simultaneous fumigation of different greenhouse areas. In some applications, it is desirable to eliminate the deposited film on the wall as far as possible, e.g. in internal combustion engines, whereas in some cases the maximum deposition is required, e.g. in agricultural sprayers (Kalantari and Tropea, 2007). Al Ashry et. al. (2009) showed that the proper unit to execute the spraying operation under greenhouse conditions is the disc sprayer after development. It has given the lowest values of volume median diameter VMD (65μm), percent of plant damage (1.26%) and highest values of number of droplets/cm^2 (295) and fungicide efficiency (86.33%). Subramanian et al. (2005) and Singh et al. (2005) also described a mini-robot to perform spraying activities, for which navigation is controlled by algorithms based on fuzzy logic. Some of researcher presented the Agrobot project, a robotic system for greenhouse cultivation of tomatoes (Shariati, 2004). In this study, characterization of a full cone spray nozzle

is presented. Spray flow rate of the nozzle is obtained as a function of incoming pressure to the nozzle. Meanwhile distribution of mean drop size, two components of drop velocity and uniformity of the generated spray are given in this study. Micro spraying takes the concept of a spray boom down to the centimeter level (Søgaard and Lund, 2005). It applies highly targeted chemicals and can treat small areas by selectively switching the jets on and off. El-Aidy (1991) reported that in Egypt, plastic tunnel greenhouses are used increasingly as a newly developed technique for vegetable or ornamental production (about 1.000 ha in 1991). Pringnitz et al. (2010) mentioned that the degree of atomization depends upon the characteristics and operating conditions of the atomizing device and upon characteristics of liquid being atomized.

OBJECTIVES

The objective of this current research was to develop the electrical hand-held hydraulic sprayer for using in controlled environment agriculture pesticides in piper crops under greenhouse conditions. As well as, applying the developed solar sprayer in small scale cultivate open Cabbage field (*Brassica oleracea var. Capitata*) under Egyptian conditions. As well as the use of photovoltaic cells for electric solar sprayer can optimize the battery duration of these equipment. Therefore this work has aimed to develop and evaluation a system to ease battery charging in conditions of field and optimizing its duration in electric sprayers using photovoltaic panels. Also, it's important to convert the "Fuel Operating System" as "Free Energy Operating System" for agriculture implementation.

MATERIALS AND METHODS

The electrical solar hydraulic sprayer was manufactured and evaluated in Agricultural Engineering Dept., faculty of Agriculture Kafrelsheikh University. The boom sprayer may able to set up in two different positions such as vertical and horizontal boom sprayer. The two pistons were constructed to change the position of the boom sprayer from vertical to horizontal set. The boom sprayer made from Aluminum in two parts and every part included of the two nozzles. The two parts of the boom sprayer carried in the lever arm to change the height of vertical boom sprayer from 1.0 m to 2.5 m height in horizontal set. The length of

each boom part is 1 m. The two parts of the boom sprayer was fixed by two pistons and the end of the piston was jointed in the frame. The 20 liter liquid tank was constructed with the valves and pipe lines into the sprayer. The dry battery with 70 Ah was connected with the centrifugal hydraulic water pump Turbo QB60 with 0.37 kW. The Dake DC/AC 1500 W inverter was connected between the electric water pump and the dry battery. The two Tee jet XR 110-3 VP nozzles oriented in the bottom and two Lechler LU110-04 nozzles set up in the top on the vertical boom position. As well as, the frame and other component of sprayer such as the hydraulic pump, battery and 20 liters' tank were set up at the three wheels as shown in figure 1. The pressure gauge and pressure transducer was mounted to test the operating pressure and controlled the spray distribution for the developed sprayer. The hand held sprayer was operated by using the DC current that converted into AC current to operate the hydraulic sprayer as shown in figure 2. The maximum operating time was measured under laboratory conditions. The developed sprayer at 200 kPa operating pressure compared to Suzuki (2.13 kW) an air assisted backpack sprayer at full air out let throttle under open field and greenhouse conditions. The dimension of greenhouse in the experimental farm was 30 x 6 x 2.6 m and it's included at 9 rows with 60 cm width. As well as the small Cabbage open field was 17 m width x 40 m long and the width for each row was 70 cm.

Procedures and tests

The spray distribution for the developed electrical hydraulic sprayer was measured under laboratory conditions at 125 kPa, 150 kPa and 200 kPa. The flow rate for each operating pressure was recorded. As well as, the vertical distribution for each two sides of the vertical boom sprayer setting was measured by using the vertical patternator in the laboratory of Agricultural Engineering Department, faculty of agriculture, kafrelsheikh University (Sehsah, 2016). The tests of coverage and spray efficiency were carried out in the experimental field in Kafrelsheikh University as shown in figure3. The solar sprayer was compared to motorized air assist knapsack sprayer model Suzuki under piper crops in greenhouse and Cabbage small cultivate field conditions. The field capacity and power requirement were measured under all treatment conditions. The food

Blue coloring was used as the deposit tracer. Dye was added to the spray tanks to provide a concentration of 1.0 mg/ml for all of the higher application rate treatments. A tank concentration of 4.0 mg/ml was used for the reduced application rate treatment, to ensure an equivalent amount of dye was applied to the test site. The deposit targets consisted of Water Sensitivity papers (WSP) harvested from a location over 30 m long of the spray site. Water Sensitivity Papers (WSP) allowed to dry and then were placed individually in collection bottles and capped. The filter papers were placed on the target holders before each treatment. The WSP was placed in one sampling piper crops line (n = 4 crops) compared to three for the deposit measurements. The final coverage rating for each target was calculated as the mean of the ratings for the two different periods. The sample from the sprayer's tank was collected for calibration of the measurement. The 100 ml of distilled water added to each WSP to wash the tracer from samples in Petri dishes. The tracer concentration in the washing solution was determined using the Dr. Lange photometer LKT. The percent recovery calculations for the field data were based on the average fluorometrically determined deposit as a percentage of the calibrated volumetric application volume rate (Sehsah et al., 2007). Determination of deposit was performed with the following equations; the symbols used are defined in the notation.

$D_e=(C * c_i.f.* q)/ (c_{ii}.s* a* m)$ [µg cm^{-2}]

$R.D = (D / T)*100$ [%]

$T= c_{ii}*V/1000$ [µg l^{-1}]

D_e	Deposition	[µg cm^{-2}]
R.D	Relative deposition	[%]
C	Photometer value (concentration)	
$c_i.f.$	Correcting factor,	[1]
q	Washing –up liquid quantity	[40 µg l^{-1}]
a	Ash	[5000 µg l^{-1}]
$c_{ii}.s$	Collector surface area	[4.5 cm^2]
m	Measuring range factor	[1]
T	Tracer application rate	[µg l^{-1}]
c_{ii}	Tracer concentration	
V	Volume application rate	[l ha^{-1}]

The deposit data were analyzed using Origin program to calculate the analysis of variance based on a general linear model for a complete randomized block which consisted of the sprayers and their site. The source of replication within each experimental block was the plants. Coverage data were analyzed similarly by rows using the mean ratings for two rating times. Homogeneity of variance tests on the data using a Levene's test indicated that the data did not need any transformations. Mean separations were compared and reported using Least Significant Differences (alpha = 0.05). Duncan's multiple range tests, Duncan-Waller, and differences of least square means produced the same comparison of mean separation as the LSD test.

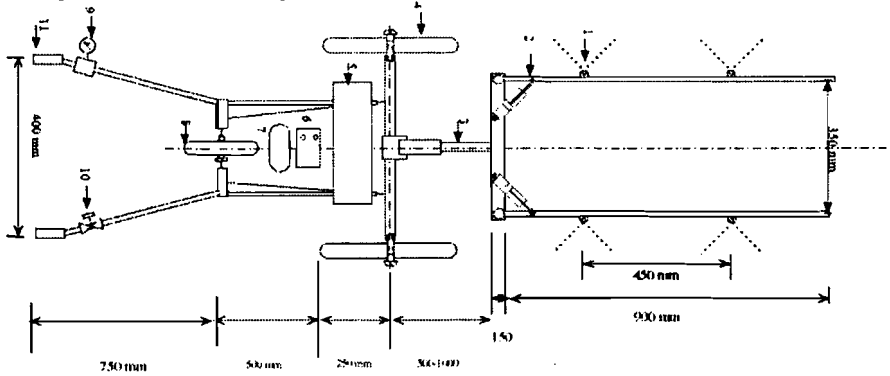

Figure 1: The diagram of the developed hydraulic sprayer

Power source of the development sprayer

The dry battery is very sensitive in the charging and needs a special charger to control the charging. The charger deliver 10 A to the battery. When a dry battery is discharged 80% and only 20% capacity is left in the battery, the overall lifetime of the battery (if not recharged at this point) is reduced a lot. This means that the battery will last longer if it is recharged with 20% capacity left. The battery can get destroyed if the battery is more than 90% discharged. This means that the battery only has to charge 80% of the 70 Ah. The chargeable time of this battery could be calculated as follow: 70Ah·0.8/10Ah/hour = 5.6 hours. The battery chargeable time 5.6 hours presupposes that the battery is 100% efficient at absorbing the charge. The battery is charged with a charge

controller and the reduction of power battery (BPR) has to receive as follow: $BPR = (1-E_2*I_2 / E_1*I_1)$

Whereas: BRP is the reduction power rate of battery, E_1 is the voltage at start operation and E_2 is the voltage after 15 min, 30 min, 45 min and one hour operation. The I_1 and I_2 value is the electric current with ampere measured at start and during the operating time respectively. The inverter model Deka 1500 converted the 0.12 kW DC power to 1.32 kW AC power to operate the Turbo QB60 hydraulic pump with power 0.37 kW. As well as the elapsed time was recorded at 80 % from the battery efficiency to start the rechargeable. The PSGI wattmeter and the multi-meter MS 345 was used to measure the power consumption directly from the inverter Deka1500. The TES-1333 solar power meter is a device which used to measure solar power (sunlight) under open field and greenhouse conditions. As well as the tests of the PV chargeable panel was treated under open field and greenhouse for one hour operation at 200 kPa operating pressure. The developed sprayer was evaluated with solar panel and without solar panel under small field and greenhouse.

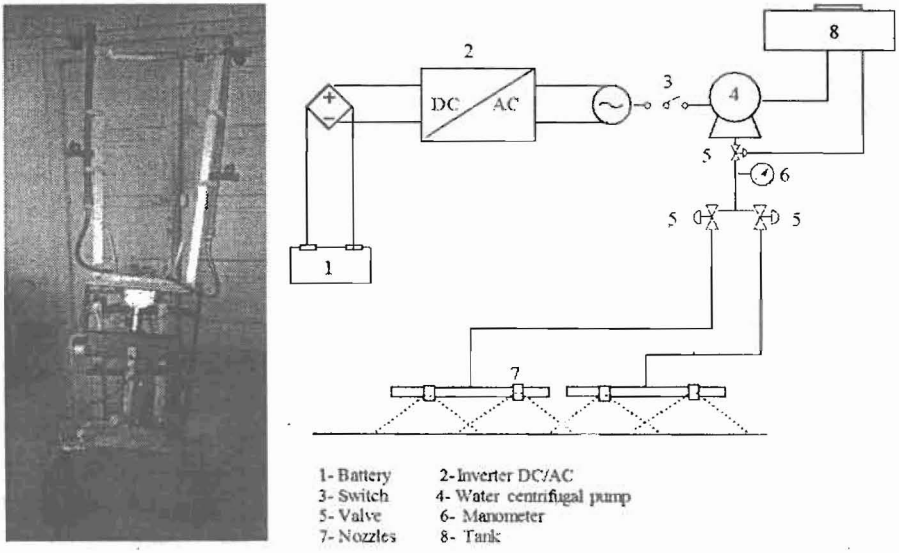

Figure 2: The diagram of the electric circuit in developed hydraulic sprayer

Figure 3: Evaluation of vertical boom site developed sprayer in piper crops under greenhouse conditions.

RESULTS AND DISCUSSIONS

The evaluation of the developed solar sprayer was tested and compared under Laboratory conditions. As well as the developed sprayer evaluated under greenhouse (Piper crops) and open field (Cabbage crops) conditions. The pattern evaluation test under laboratory conditions for the developed solar sprayer at vertical boom set in both left and right side indicated as shown in figure 4 under different operating nozzle pressure 125 kPa, 150 kPa and 200 kPa. The pattern percentage values increased due to increase the operating pressure. The pattern percentages in right side were 31.24 %, 35.26 % and 37.18 % for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures at 1.5 m height respectively. The pattern percentages in left side were 33.99 %, 32.34 %and 33.69 % for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures at 1.5 m height respectively. The pattern percentage increased from 0.5 m height to 1.5 m height for vertical boom in both left and right side. On other hand, the pattern percentage decreased after 1.5 m height to 2.5 m height. This result indicated that the developed sprayer gave the high pattern percentages at 1.5 m height and operating pressure 200 kPa for both vertical boom sides. As well as, there are non-significant different between left and right side in vertical boom set. The flow rate measured values from both orientation nozzles side in vertical boom and horizontal set indicated in table 1 under laboratory conditions. The total flow rates

in vertical boom set were 2.11 L.min $^{-1}$, 3.12 L.min $^{-1}$and 3.88 L.min $^{-1}$ for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. As well as, the total flow rate in horizontal boom set were 3.2 L.min $^{-1}$, 3.71 L.min $^{-1}$and 4.28 L.min $^{-1}$ for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. It is noticed that the flow rate in horizontal boom set produced high values compared to vertical boom position. This result due to the gravitational in vertical set that reduced the flow of spray liquid. Also, the sprayer in horizontal boom position will be re-feeding more than in vertical boom set. As well as the flow rate for each oriented nozzles in boom sprayer in two positions gave not significant different in both left and right side of boom as shown in table 1.

Field experimental result

The results of the current research presented that it may able to use the developed sprayer under greenhouse (Piper crops) and open field (Cabbage crops). Deposition for developed solar sprayer and knapsack sprayer indicated in table 2. The horizontal boom set gave high value of deposition compared to vertical boom set as shown in figure 5. As well as, the increasing of operating pressure tends to increase the deposition values for developed solar sprayer. The deposit spray values under open field conditions were 0.133μg/cm^2, 0.187μg/cm^2 and 0.208μg/cm^2 for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. As well as, the deposit values under greenhouse conditions were 0.09 μg/cm^2, 0.12μg/cm^{2}and 0.16μg/cm^2 for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. Also, the air assist knapsack sprayer gave high deposit values compared to the developed sprayer at low operating pressure 125 kPa and 150 kPa under all treatment conditions. On the other hand, the developed solar sprayer at 200 kPa operating pressure gave non-significant different of deposit compared to knapsack sprayer under open field condition. The deposit value was 0.208 μg/cm^{2}and 0.218 μg/cm^2 for developed sprayer at 200 kPa operating pressure and full air outlet knapsack sprayer respectively. Figure 6 indicate the coverage percent for developed sprayer under greenhouse (vertical boom set) and open field (horizontal boom set position) conditions. The operating of the developed solar sprayer with horizontal set gave high values of coverage percent compared to vertical

boom set. Also, increasing of the operating nozzles pressure tends to increase the coverage percent in both greenhouse and open field conditions. The coverage percent values under open field conditions were 37.8%, 39.1% and 44.5% for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. As well as, the coverage percent values under greenhouse conditions were 27.8 %, 29.7% and 33.8 % for 125 kPa, 150 kPa and 200 kPa operating nozzle pressures respectively. On the other hand, the developed solar sprayer operating at 200 kPa pressure gave 44.5 % of coverage percent compared to 49.3 % for knapsack sprayer under open field condition as shown in figure 7.

Power requirement for developed sprayer

The power requirement for the development solar sprayer was measured and recorded under all treatment conditions. It's noticed that the increasing of the operating pressure tends to increase the power requirement to operate the hydraulic pump in development sprayer. The power consumed was 0.26 kW, 0.28 kW and 0.30 kW at 125 kPa, 150 kPa and 200 kPa respectively. As well as the battery power reduction rate displayed in figure 8 at 200 kPa operating pressure after 60 min operation time under open field and greenhouse conditions. It's noticed that the reduction rate of battery power increased under greenhouse conditions compared to small open field at 200 kPa operating pressure. The battery power reduction rates for 60 min operation time were 0.081 and 0.192 without PV panel charger under small open field and greenhouse respectively. As well as the battery power reduction rate were 0.051 and 0.164 with PV panel charger under small open field and greenhouse respectively. This result may be due to the solar radiation under greenhouse was less than the solar radiation in small open field condition as shown in table 3. The solar radiation effected on the production of electric power from the panel that used to charge the dry battery. It could be reduce the reduction power percentage by using two PV charger panel in electric solar sprayer under greenhouse and small open conditions. The increasing of the operating time for solar development sprayer tends to reduce the operating pressure and the power requirement may be decreased. The developed sprayer may able to operate for around 215 min without recharging the battery at operating pressure 200 kPa.

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Table 1: Presented the flow rate of the vertical and horizontal position for four different nozzles in developed sprayer

Vertical boom position

Pressure, kPa	Flow-rate, l min $^{-1}$			
	Right		Left	
	XR110-3	LU110-04	XR110-3	LU110-04
125	0.62	0.39	0.62	0.48
150	0.97	0.61	0.90	0.64
200	1.12	0.86	1.06	0.48

Horizontal boom position

Pressure, kPa	Flow-rate, l min $^{-1}$			
	Right		Left	
	XR110-3	LU110-04	XR110-3	LU110-04
125	0.98	0.65	0.94	0.63
150	1.11	0.78	1.09	0.73
200	1.27	0.89	1.25	0.87

Table 2: Spray deposit on piper and cabbage leaves using developed and air assist knapsack sprayers.

Treatment	Open field deposit, µg/cm^2	Greenhouse deposit, µg/cm^2	Flow rate, L min^{-1}
Developed sprayer at 125 kPa	0.1331	0.0929	1.63
Developed sprayer at 150 kPa	0.1879	0.1200	1.89
Developed sprayer at 200 kPa	0.2081	0.1601	2.16
Air assist knapsack sprayer	0.2134	0.1985	1.84

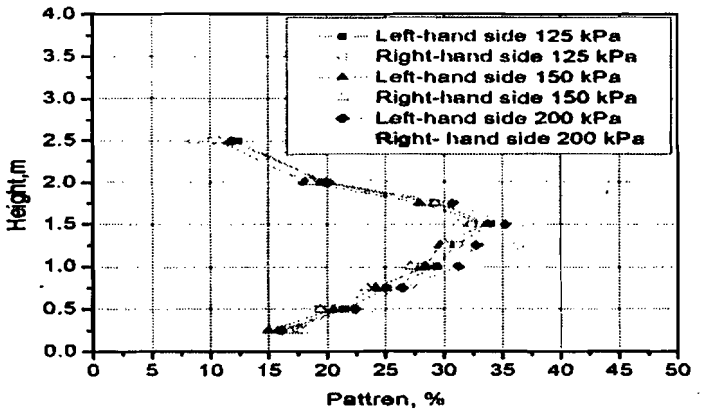

Figure 4: Left-and right-hand side spray distribution (cm water per 25 cm height) measured on a vertical patternator for a vertical sprayer at 125 kPa, 150 kPa and 200 kPa operating pressure.

Table 3: The measured values of solar radiation and temperature under open field and Greenhouse conditions

Date	Time	Solar radiation in open field, W/m^2	Temperature in open field, °C	Solar radiation in Greenhouse, W/m^2	Temperature In Greenhouse, °C
5/3/2015	9:30	672.2	19.3	206.2	43.3
5/3/2015	10:30	602.9	19.3	252.6	44.6
5/3/2015	11:30	639.1	23.0	245.3	49.0
5/3/2015	12:30	615.4	21.1	329.2	45.1
7/3/2015	9:30	551.1	19.2	256.7	43.2
7/3/2015	10:30	651.6	18.8	272.4	44.8
7/3/2015	11:30	667.4	24.7	295.1	48.7
7/3/2015	12:30	581.1	24.1	351.8	48.1

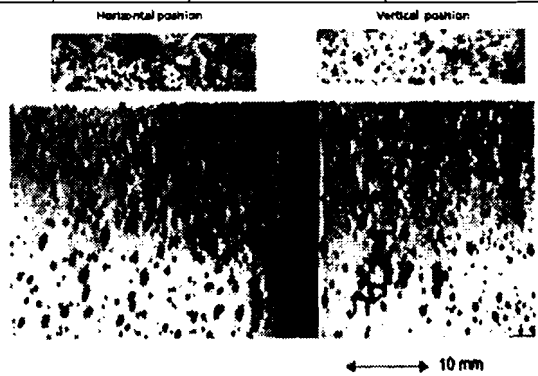

Figure 5: The deposition for horizontal boom and vertical boom setting.

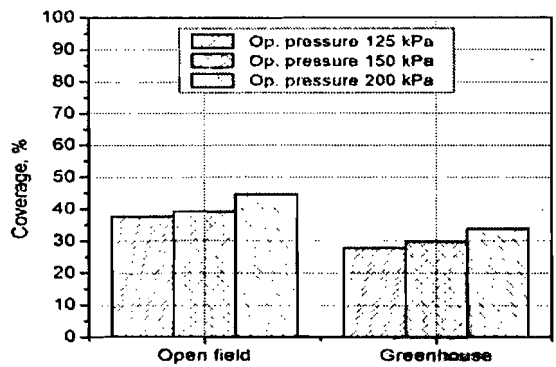

Figure 6: The coverage percent for developed sprayer under greenhouse (vertical boom set) and open field (horizontal boom set position) conditions.

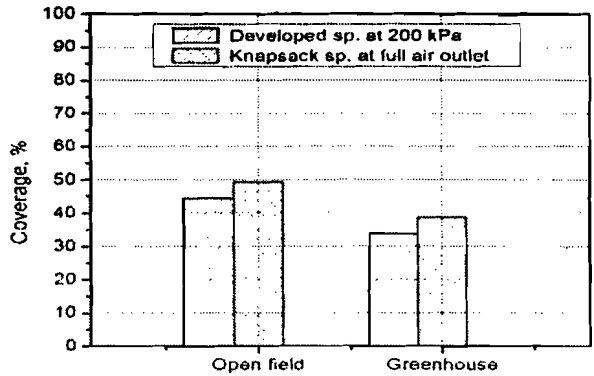

Figure 7: The coverage percent for developed sprayer and air assist knapsack sprayer under greenhouse (Piper crops) and open field (Cabbage crops) conditions.

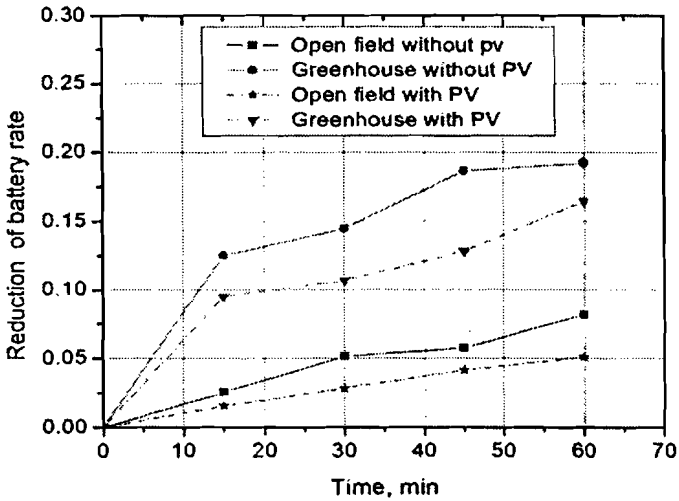

Figure 8: The battery power reduction rate for developed electric sprayer at 200 kPa operating pressure under open field and greenhouse conditions.

SUMMARY AND CONCLUSIONS

The result indicated the electrical hydraulic sprayer may able to use and apply in the greenhouse and small cultivate open field under local conditions. The pattern percentage decreased after 1.5 m height to 2.5 m

height. This result indicated that the developed sprayer gave the high pattern percentages at 1.5 m height and operating pressure 200 kPa for both vertical boom sides. As well as, there are non-significant different between left and right side in vertical boom set. The developed solar sprayer at 200 kPa operating pressure gave non-significant different of deposit compared to knapsack sprayer under open field condition. The deposit value was 0.208μg/cm^{2}and 0.218μg/cm^2 for developed sprayer at 200 kPa operating pressure and full air outlet knapsack sprayer respectively. The air assist knapsack sprayer gave high deposit values compared to the developed sprayer at low operating pressure 125 kPa and 150 kPa under all treatment conditions. Also, the operating pressure tends to increase the power requirement to operate the hydraulic pump in development sprayer. As well as the reduction rate of battery power increased under greenhouse conditions compared to small open field at 200 kPa operating pressure. In this condition of work using the 200 kPa, probably the operator will not have problems in relation to the length of the battery, once itself has operational capacity enough for performing the operation along a day. However, in case the operator increases the pressure or the time of spraying, the battery may end before the end of day. Yet with the use of photovoltaic cells, occurs the increase of the sprayer autonomy, reducing the probability of the battery ending up in the field. It is known that in spraying, whenever it is possible, it is common to apply low volume of spray, in order to increase the operational. In remote places or with difficult access to electric power net, it is possible to use the photovoltaic system for charging these sprayers. It could be recommended that the centrifugal pump may change to the DC membrane pump which as available in the Egyptian market. This pump goes to reduce the price of the electrical sprayer and their maintenance. As well as, it will be better if the sprayer mounted with a Robot in greenhouse.

Acknowledgment

The author would like to extend their thanks to all staff member in experimental research field, Kafrelsheikh University, Egypt.

REFERENCES

El-Ashry, A.S., H.A. El-Gendy and M.H. Abo El-Naga (2009), Development and performance evaluation of a greenhouse pesticides sprayer . The 16th Annual Conference of the Misr Society of Ag. Eng., 25 July, 2009

Hilz, E., and A.W.P. Vermeer (2013), Spray drift review: The extent to wich a formulation can contribute to spray drift reduction. Crop Protection 44: 75-83.

Jivrag, A., V. Chawre, and A. Bhagwat (2011), Solar Operated Multiple Granulated Pesticide Duster" Proceedings of the World Congress on Engineering, Vol 3, July 6-8,. London, U.K

Kalantari, D., and C.Tropea. (2007), Spray impact onto flat and rigid walls: Empirical characterization and modeling. International Journal of Multiphase Flow, 33(5): 525-544.

Miller, P. C. H., and D. Hadfield (1989), A simulation model of the spray drift from hydraulic nozzles. J. Agr. Eng. Res. 42(2): 135-147.

Oerke, E.C. (2006), Crop losses to pests. The Journal of Agricultural Science 144: 31-43.

Pringnitz, B. A., M.Hanna, and J.Ellerhoff (2010), Selecting the correct nozzle to reduce spray drift. www.weeds.iastate.ed (accessed March 2, 2012).

Rao. V. V., S Mathapati and B. Amarapur (2013) Multiple Power Supplied Fertilizer sprayer International Journal of Scientific and Research Publications, Volume 3, Issue 8, August

Rowe, D.E.,S. Malone, and Q. L. Yates (2000), Automated greenhouse spray system for increased safety and flexibility .Journal of Crop Sci. 40:1176–1179.

Sammons, P.J., F.Tomonari, and A.Bulgin (2005), Autonomous Pesticide spraying robot for use in a greenhouse. Australian

Conference on Robotics and Automation, pp. 1-9, ISBN 0-9587583-7-9, December 2005, Sydney, Australia.

Shariati, I. (2004), Design and manufacturing a sample of mechanical arm of robot in order to distinguish fruit in specific direction. M. Sc. Thesis. Agricultural machinery dept. of Tehran University, Iran.

Singh, S., W.S.Lee, and T. F.Burks (2005), Autonomous robotic vehicle development for greenhouse spraying. Transactions of the ASAE, 48(6): 2355-2361.

Søgaard, H. T. and I. Lund. (2005), Investigation of the accuracy of a machine vision based robotic micro spray system. In Proc. 5th European conference on Precision Agriculture, 8-11 June., ed. J.

Subramanian, V., T.F. Burks, and S.Singh. (2005), Autonomous greenhouse sprayer vehicle using machine vision and radar for steering control. Applied Engineering in Agriculture, 21(5):

Sehsah, E., G. Baecker and S. Kleisinger (2004c), Evaluation of an experimental sprayer with rotary atomizers by air characteristics, soil sedimentation, deposition and vertical drift. International Conference Environmentally Friendly Spray Application Techniques 4-6 October, 2004c – Warsaw, Poland.

Sehsah E.M.E. (2005), Application techniques for biological crop protection in Orchards and vineyards. Ph.D thesis, Hohenheim University, ISDN: 3-86186-484-3 Vorlag Grauer Stuttgart Germany.

Sehsah E.M.E. (2007), Study effect of forward speed and nozzles types on spray characteristics of air assistance hydraulic sprayer, Misr J.Ag.Eng., 24 (1): 75-87.

Sehsah E.M.E. and S. Kleisinger (2007), Effect of low pressure liquid atomizers usage in biological pest control, Misr J.Ag.Eng., 24 (1): 62-74.

Sehsah E.M. (2016): Vertical patternator for evaluation of hydraulic sprayer, Misr J.Ag.Eng., 33 (4): 1239-1254.

الملخص العربى

تطوير آلة رش كهربائية للصوب الزراعية و المزارع الصغيرة

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تهدف هذه الدراسة الى البحث فى أمكانية تطوير آلة رش تعمل بالتيار الكهربائى والتى يمكن أستخدامها للحيازات الصغيرة و الصوب الزراعية و بخاصة الصوب التى تستعمل فى زراعة محاصيل الخضر المتسلقة مثل الفلفل وغيرها من محاصيل الخضر. كما أن استعمال الخلايا الفولتية فى تشغيل الآلة يؤدى ايضا لتقيل الأعتماد على البترول كمصدر للطاقة لتشغيل آلات الرش حيث تعتبر عملية الرش من العمليات المؤثرة فى انتاجية المحصول و تحديد تكاليف أنتاجة. ولقد تم تصنيع وتطوير الآلة بقسم الهندسة الزراعية والتى تتكون من هيكل من الحديد محمول على ثلاثة عجلات ، أثنان منها فى الأمام و العجلة الثالثة فى الخلف و مثبت عليه طلمبة هيدروليكية قدرة ٠.٣٩ ك. وات تعمل بالتيار المتردد و متصلة بعاكس للتيار طراز Deka Inverter 1500 قدرة ١٥٠٠ وات لتحويل التيار المستمر من البطارية الجافة سعة ٧٠ أمبير ساعة و المثبته بالآلة و التى يتم شحنها بواسطة شاحن شمسى PV قدرة ٣٦ وات ، كما تحتوى الآلة على خزان سعة ٢٠ لتر متصل بالطلمبة طراز Turbo QB60 و صمامات تحكم ميكانيكية متصلة مع مواصير سائل الرش المثبت بحامل البشابير. كما تم تطويرحامل البشابير وتصنيعة من الألومنيوم ليعمل على الوضع الرأسى و الأفقىبواسطة مكبسين ليناسب ظروف الصوب و محصول الفلفل المتسلق بأرتفاع ٢.٤ م و الذى يتم التحكم فى الوضع الرأسى بواسطة ذراع تلسكوبى كما أن الوضع الأفقى لحامل البشابيرذو عرض تشغيل ١.٥ م للرش وذلك لرش محصول الكرنب . أيضا تم تركيب عدد ٢ فونيه طراز Tee jet XR 110-3 VP فى أعلى حامل البشابيرعلى الجانبين و عدد ٢ فونيه طراز Lechler LU110-04 فى الجانب السفلى و ذلك لضمان معدل تصرف متزن على جانبى حامل البشابير. حيث تم قياس تركيز سائل الرش بواسطة جهاز Photometer Dr. Lange LK. أيضا استعمل جهاز طراز PSGI لقياس القدرة المطلوبة للتشغيل عند كل ضغط و استعمل جهازTES-1333 solar power meter لقياس شدة الأشعاع تحت ظروف الحقل و الصوبة. و لتقييم الآلة معمليا تم قياس التوزيع الرأسى عند تشغيلها على ثلاثة ضغوط هى ١٢٥ ك.بسكال و ١٥٠ ك.بسكال و ٢٠٠ ك.بسكال حيث أستعمل الموزع الرأسى لتقدير ذلك . أيضا تم قياس معدل التصرف عند كل ضغط وعند تشغيل الآلة فى الوضع الرأسى و الأفقى لحامل البشابير. و قد أجريت المعاملات التالية لأختبار و تقييم أداء الآلة المطورة حقليا ذلك بقياس التوزيع و نسبة التغطية لرش محصول الكرنب فى حقل صغيره أبعادها ٤٠ x ١٧ م و بعرض للخط ٧٠ سم حيث كان وضع حامل البشابير أفقيا و عند ضغوط التشغيل السابقة ١٢٥ ك.بسكال و ١٥٠ ك.بسكال و ٢٠٠ ك.بسكال.

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بينما تم أختبار و تقييم الآلة المطورة تحت ظروف الصوبة الزراعية و المنزرعة بمحصول الفلفل المتسلق و حيث كانت الصوبة ذات ابعاد ٩x٣٠x٣ م بعرض للخط ٦٠ سم و عند تشغيل الآلة المطورة و أختبارها للوضع الرأسى لحامل البشابير وعند نفس ضغوط التشغيل ١٢٥ ك.بسكال و ١٥٠ ك.بسكال و ٢٠٠ ك.بسكال و بأرتفاع ٢ م من سطح التربة ، ولقد تم مقارنة المعاملات السابقة من تشغيل الالة المطورة لمعاملات التشغيل فى حقل الكرنب و الصوبة الزراعية موضع الدراسة بآلة الرش الظهرية طراز Suzuki air assist knapsack sprayer عند وضع كامل لفتحة خروج الهواء بآلة Suzuki air assist knapsack sprayer. و فى دراسة لتقييم انخفاض قدرة البطارية لظروف التشغيل فى حقل الكرنب و تحت ظروف الصوبة الزراعية تم أختبارالآلة المطورة و ذلك بتشغيل لفترات ٠.٢٥ ساعة و ٠.٥ ساعة و ٠.٧٥ ساعة و ١ ساعة من بأستعمال الشاحن الشمسىPV وعند عدم استعمال الشحن الشمسى PV لتقدير نسبة انخفاض قدرة البطارية والتى تعتبر مصدرالقدرة للآلة الرش المطورة. و قد اتضح من النتائج أنه لا يوجد فروق معنوية فى نسبة التوزيع الرأسى لسائل الرش للآلة الرش الكهربائية المطورة عند تشغيل حامل البشابير فى الوضع الرأسى كما لوحظ أنه بزيادة ضغط التشغيل يزداد نسبة التوزيع الرأسى لأرتفاع ١,٥ م من أرتفاع محصول الفلفل المتسلق داخل ظروف الصوبة الزراعية، حيث بلغت قيمتها ٣٧.٨% و٣٩.١% و٤٤.٥ % عند ضغوط تشغيل لآلة الرش الكهربائية المطورة ١٢٥ ك.بسكال و ١٥٠ ك.بسكال و ٢٠٠ ك.بسكال على الترتيب. من جانب آخر وجد أن نسبة التغطية قد بلغت ٤٤.٥ % لآلة الرش المطورة عند تشغيلها عند ضغط ٢٠٠ ك.بسكال مقارنة بالقيمة ٤٩.٣ % لآلة الرش Suzuki air assist knapsack sprayer تحت ظروف الحقل. بينما بلغت نسبة التغطية ٢٧.٨% و٢٩.٧ % و٣٣.٨% عند ضغوط تشغيل لآلة الرش الكهربائية المطورة ١٢٥ ك.بسكال و ١٥٠ ك.بسكال و ٢٠٠ ك.بسكال على الترتيب. و لقد بينت النتائج أيضا أن زيادة ضغوط التشغيل أدت الى زيادة القدرة المطلوبة من نظام PV لأنتاج الطاقة الموجود بالآلة المطورة حيث بلغت قيمتها ٠.٢٦ ك.بسكال و ٠.٢٨ ك.بسكال و ٠.٣ ك.بسكال عند ضغط سائل الرش ١٢٥ ك.بسكال و ١٥٠ ك.بسكال و ٢٠٠ ك.بسكال على الترتيب. أيضا وجد أن معدل أنخفاض قدرة البطارية للشحن خلال ساعة واحدة من التشغيل ٠.٠٥١ و ٠.١٦٢ لكل من ظروف التشغيل لرش محصول الكرنب فى الحقل و لرش محصول الفلفل فى الصوبة عند الأعتماد على نظام PV لأنتاج الطاقة الموجود بالآلة المطورة بينما بلغت قيمتها ٠.٠٨١ و ٠.١٩١ لرش محصول الكرنب فى الحقل و لرش محصول الفلفل فى الصوبة عند عدم استخدام نظام PV لأنتاج الطاقة الموجود بالآلة المطورة. و يتضح مما سبق أنه يمكن الأعتماد على نظام PV لأنتاج الطاقة الموجود بالآلة المطورة لشحن البطارية و أطلة فترة استخدامها تحت ظروف الحقل بينما عند تشغيل آلة الرش المطورة تحت ظروف الصوبة يمكن زيادة عدد أللواح الشحن الشمسى PV لأنتاج الطاقة. كما لوحظ أن آلة الرش المطورة و التى تعمل بواسطة التيار الكهربى أو الخلايا الفولتية تحتاج للشحن بعد مدة و أن اقصى فترة تشغيل كانت ٣ ساعات و ٣٥ دقيقة عند ضغط ٢٠٠ ك.بسكال.